

The finite element method II

In FEM I we derived basis functions of arbitrary order for the rod model:

$$\frac{d}{dx} \left(EA \frac{du}{dx} \right) + q(x) = 0$$

u specified at boundary or
 $\frac{AEdu}{dx}$ ✓ ✓ ✓

⇒ approximation inside element e

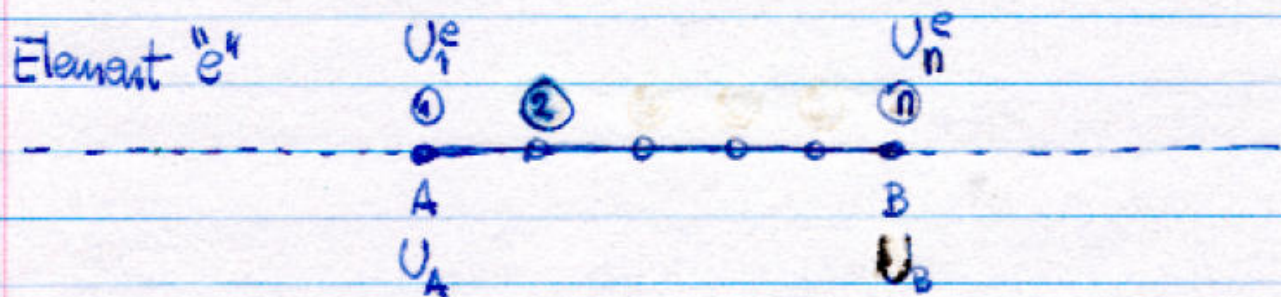
$$u_e(x) = \sum_{i=1}^n \phi_i^e(x) U_i^e$$

$$x_A < x < x_B$$

Properties of $\phi_i^e(x)$

- $\phi_i^e(x_j) = \delta_{ij} \quad j=1, \dots, n$
- $\sum_{i=1}^n \phi_i(x) = 1 \quad \forall x \quad x_A < x < x_B$

Today: use this approximation to solve Ritz approximation within element "e"



"Element boundary conditions":

$$u(x_1^e) = U_1^e$$

$$u(x_n^e) = U_n^e$$

$$AE \frac{du}{dx} \Big|_{x=x_1^e} = P_1^e$$

$$AE \frac{du}{dx} \Big|_{x=x_n^e} = P_n^e$$

PVD (alternatively PMPE)

$$\int_{x_1^e}^{x_n^e} \int_A \delta \epsilon dA dx = \int_{x_1^e}^{x_n^e} q(x) \delta u dx + \sum P_k^e \delta u(x_k^e)$$

$$\int_{x_1^e}^{x_n^e} EA \frac{du}{dx} \delta \frac{du}{dx} dx = \int_{x_1^e}^{x_n^e} q(x) \delta u dx + \sum P_k^e \delta u(x_k^e)$$

$$\int_{x_1^e}^{x_n^e} EA \frac{du}{dx} \frac{d}{dx} \delta u dx = \int_{x_1^e}^{x_n^e} q(x) \delta u dx + \sum P_k^e \delta u(x_k^e)$$

Replace approximation inside element:

$$u_e = \sum_{i=1}^n \phi_i^e(x) U_i^e \quad \delta u_e = \sum_{i=1}^n \phi_i^e(x) \delta U_i^e$$

$$\frac{du_e}{dx} = \sum_{i=1}^n \frac{d\phi_i^e(x)}{dx} U_i^e \quad \frac{d\delta u_e}{dx} = \sum_{i=1}^n \frac{d\phi_i^e(x)}{dx} \delta U_i^e$$

PVD

$$\delta W_I^e = \int_{x_1^e}^{x_n^e} EA \left(\sum_{i=1}^n \frac{d\phi_i^e}{dx} U_i^e \right) \left(\sum_{j=1}^n \frac{d\phi_j^e}{dx} \delta U_j^e \right) dx$$

$$= \int \delta U_j^e \underbrace{\left[\int_{x_1^e}^{x_n^e} EA \frac{d\phi_j^e}{dx} \frac{d\phi_i^e}{dx} dx \right]}_{K_{ji}^e} U_i^e$$

$$\delta W_E^e = \int_{x_1^e}^{x_n^e} q(x) \sum_{i=1}^n \phi_i^e \delta U_i^e dx + \sum_{l=1}^n P_l^e \underbrace{\phi_l^e(x_l)}_1 \delta U_l^e$$

$$= \delta U_j^e \underbrace{\left[\int_{x_1^e}^{x_n^e} q(x) \phi_j^e dx + \sum P_j^e \right]}_{R_j^e}$$

$$\delta W_I = \delta W_E \dots$$

$$\delta U_j^e K_{ji}^e U_i^e = \delta U_j^e R_j^e$$

$$\delta U_j^e [K_{ji}^e U_i^e - R_j^e] = 0 \quad \forall \delta U_j^e \text{ (admissible)}$$

↔

$$K_{ji}^e U_i^e - R_j^e = 0$$

Stiffness matrix:

$$K_{ij}^e = \int_{x_i^e}^{x_n^e} AE \frac{d\phi_i^e}{dx} \frac{d\phi_j^e}{dx} dx$$

- K can be computed given element type ("n") and A, E inside element.
- $K \in \mathbb{R}^{n \times n}$
- K symmetric
- K_{ij}^e can be interpreted as the force needed on node "j" when a unit displacement is applied at node "i".

- K_{ij} is singular why?

Force vector

$$R_i^e = \int_{x_1^e}^{x_n^e} q^e(x) \phi_i^e dx + P_i^e$$