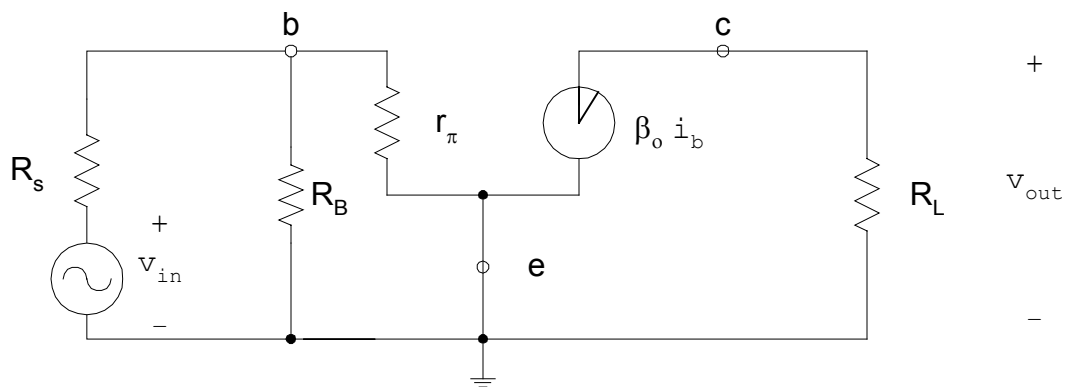
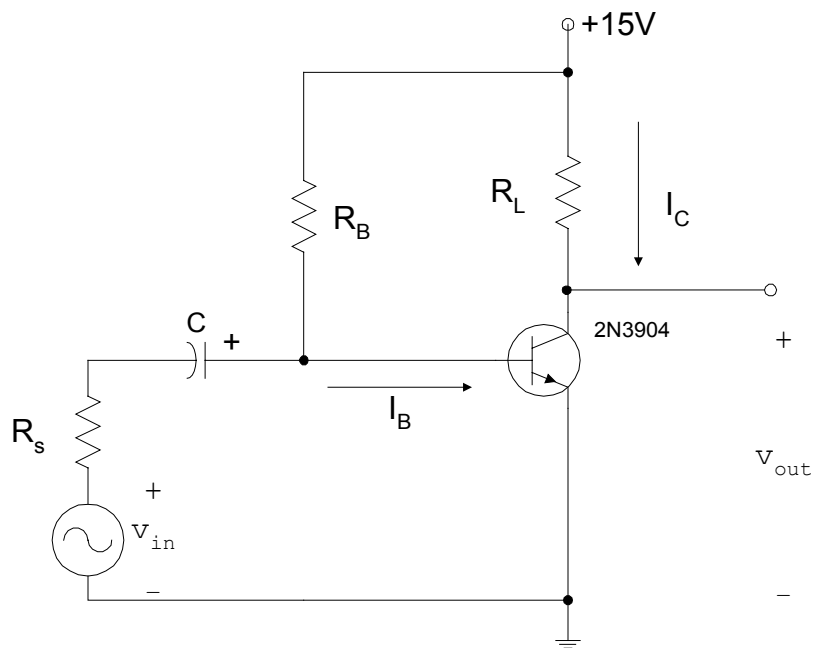


# CONFIGURACIONES DEL AMPLIFICADOR DE TRANSISTOR CON CIRCUITOS EQUIVALENTES HÍBRIDO- $\Pi$

## AMPLIFICADOR DE EMISOR COMÚN

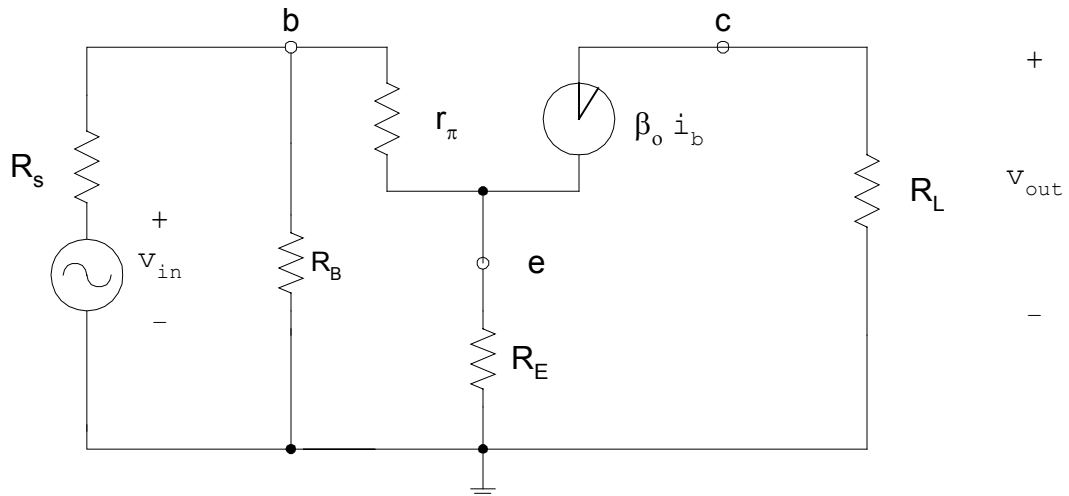
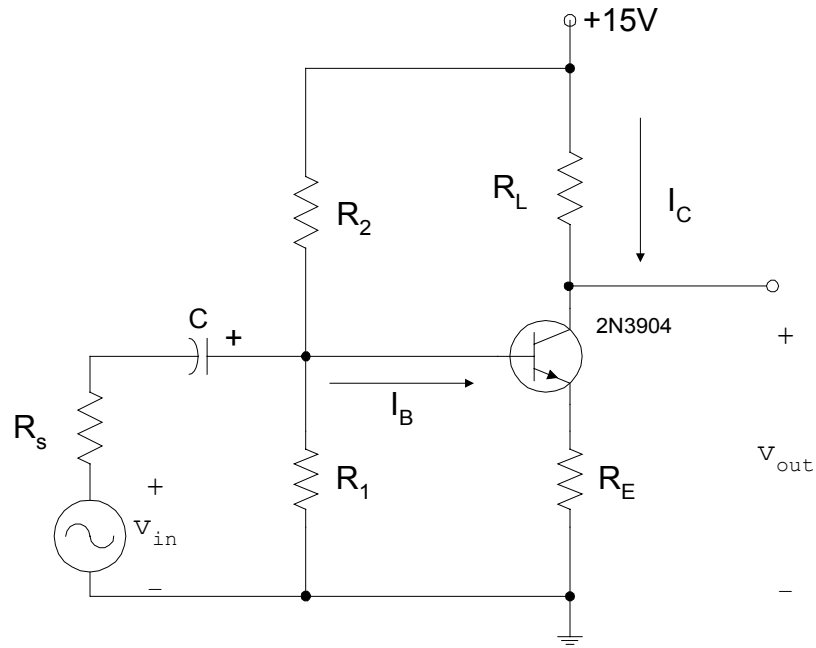


$$A_v = \frac{v_{out}}{v_{in}} = \frac{-\beta_o i_b R_L}{i_b [R_s + r_\pi]} = \frac{-\beta_o R_L}{R_s + r_\pi}$$

$$\text{si } R_s \ll r_\pi \text{ entonces } A_v = \frac{-\beta_o R_L}{\frac{\beta_o}{g_m}} = -g_m R_L$$

CONFIGURACIONES DEL AMPLIFICADOR DE TRANSISTOR CON CIRCUITOS EQUIVALENTES HÍBRIDO-II

AMPLIFICADOR DE EMISOR COMÚN CON RESISTENCIA DE DEGENERACIÓN DE EMISOR

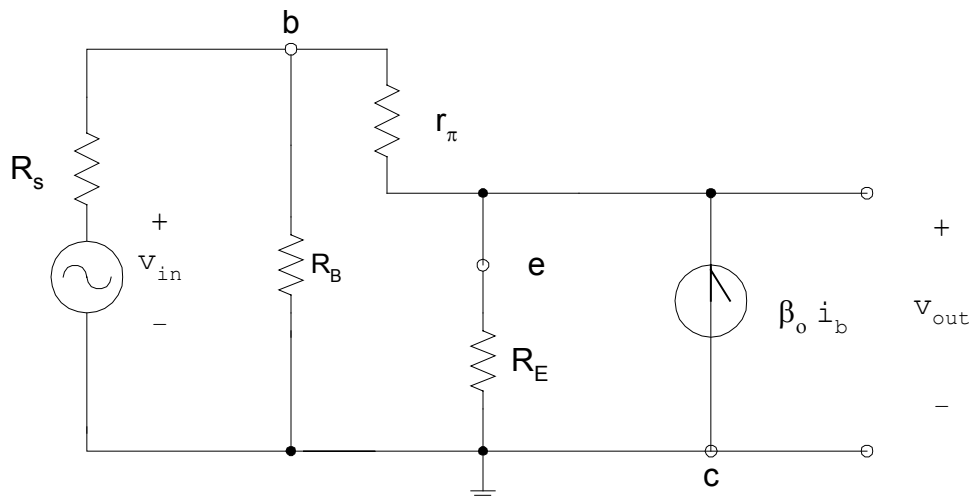
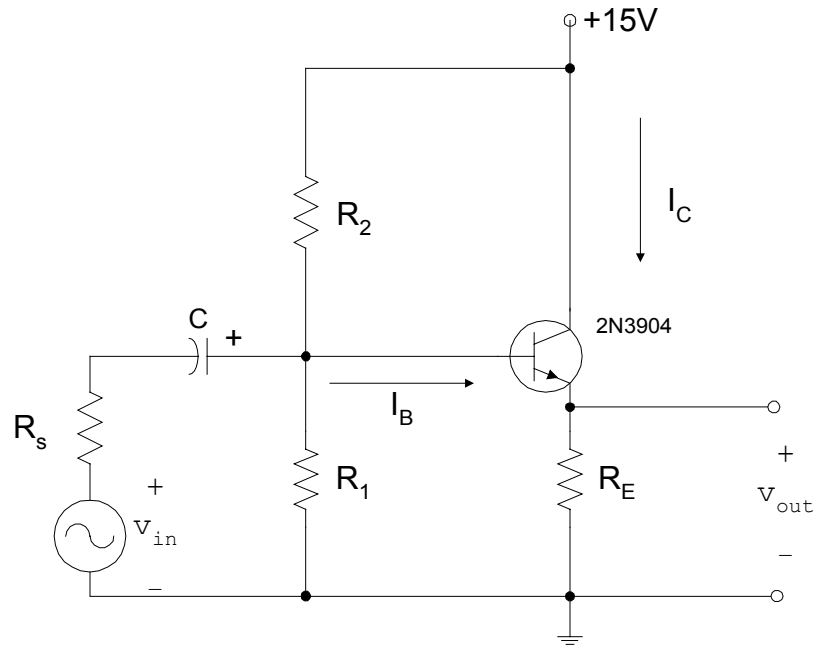


$$A_v = \frac{v_{out}}{v_{in}} = \frac{-\beta_o i_b R_L}{i_b [R_s + r_\pi + (\beta_o + 1)R_E]} = \frac{-\beta_o R_L}{R_s + r_\pi + (\beta_o + 1)R_E};$$

si  $R_s + r_\pi \ll (\beta_o + 1)R_E$ ; entonces  $A_v \approx -R_L / R_E$

CONFIGURACIONES DEL AMPLIFICADOR DE TRANSISTOR CON CIRCUITOS EQUIVALENTES HÍBRIDO- $\pi$

AMPLIFICADOR DE COLECTOR COMÚN [SEGUIDOR DE EMISOR]



$$A_v = \frac{v_{out}}{v_{in}} = \frac{(\beta_o + 1)i_b R_E}{i_b [R_s + r_\pi + (\beta_o + 1)R_E]} = \frac{(\beta_o + 1) R_E}{R_s + r_\pi + (\beta_o + 1)R_E};$$

si  $R_s + r_\pi \ll (\beta_o + 1)R_E$ ; entonces  $A_v \approx 1$